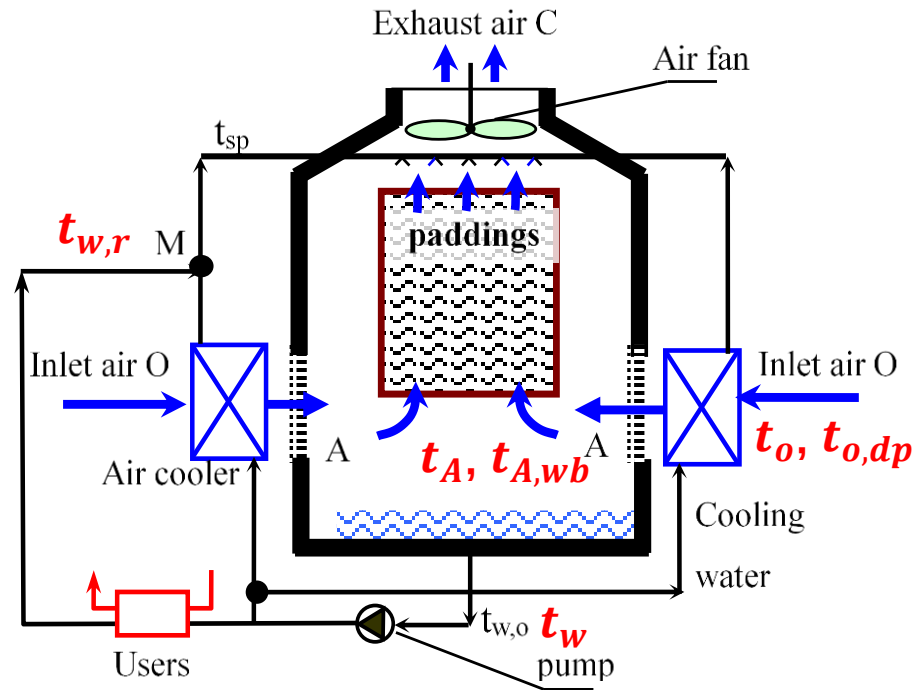


Performance of indicators for IEC water chillers

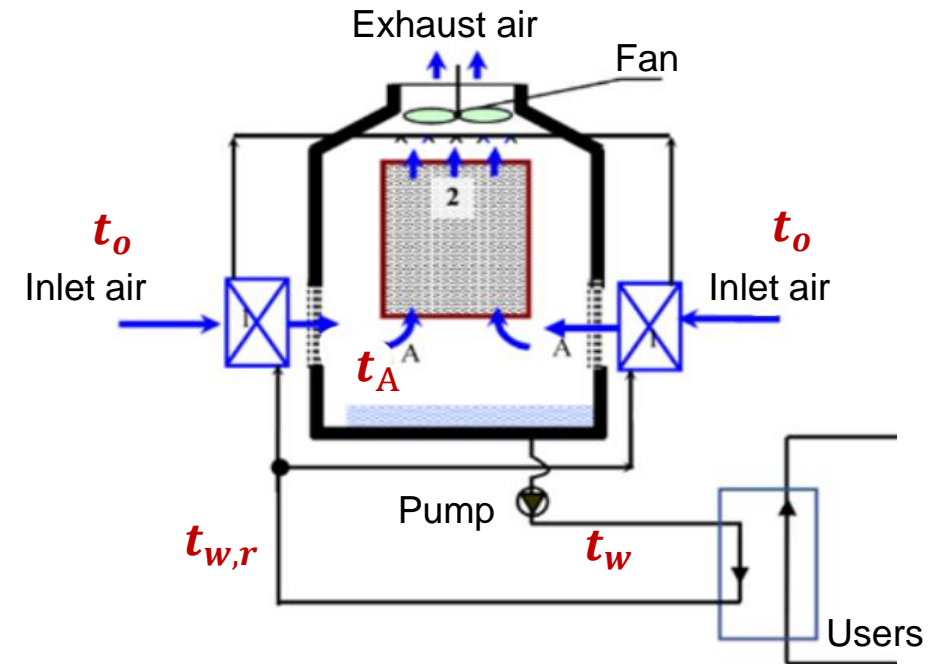
Ce Zhao, Xiaoyun Xie
Tsinghua University, Beijing, China
2022.10

IEC water chiller processes

parallel-connected IEC water chillers



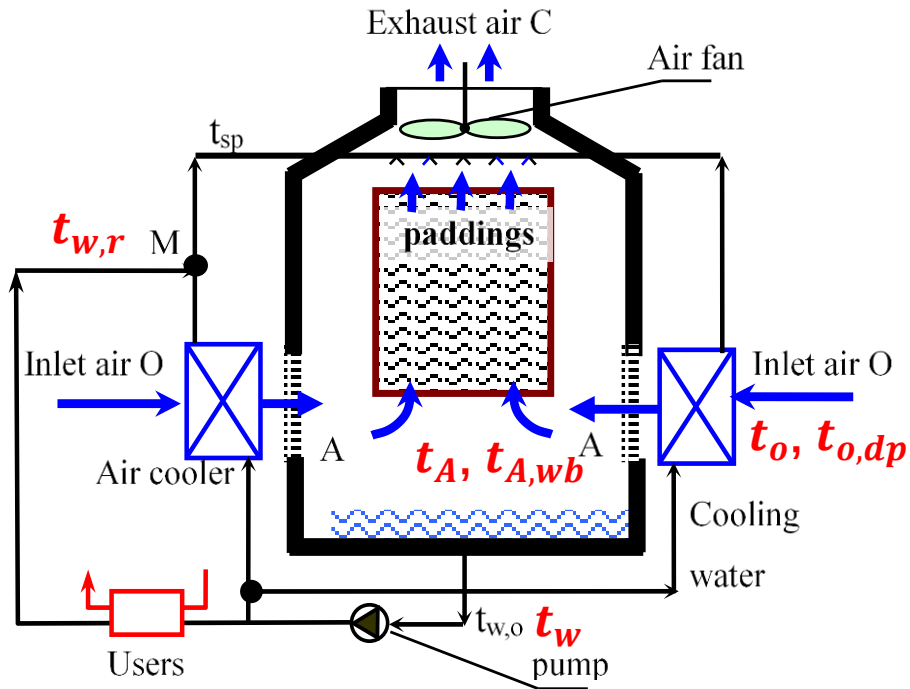
series-connected IEC water chillers



- Suitable indicators are expected with features affected by its own NTU and the flowrate ratio rather than climate conditions.

Define suitable indicators for IEC water chiller processes

- The indicators should better be stable or vary slightly with climate conditions.
- Two ways to indicate the IEC water chillers in this report:



- Only define one efficiency - Dew point temperature efficiency, to express the cooling performance.

$$\eta_{dew} = \frac{t_{w,r} - t_w}{t_{w,r} - t_{o,dp}}$$

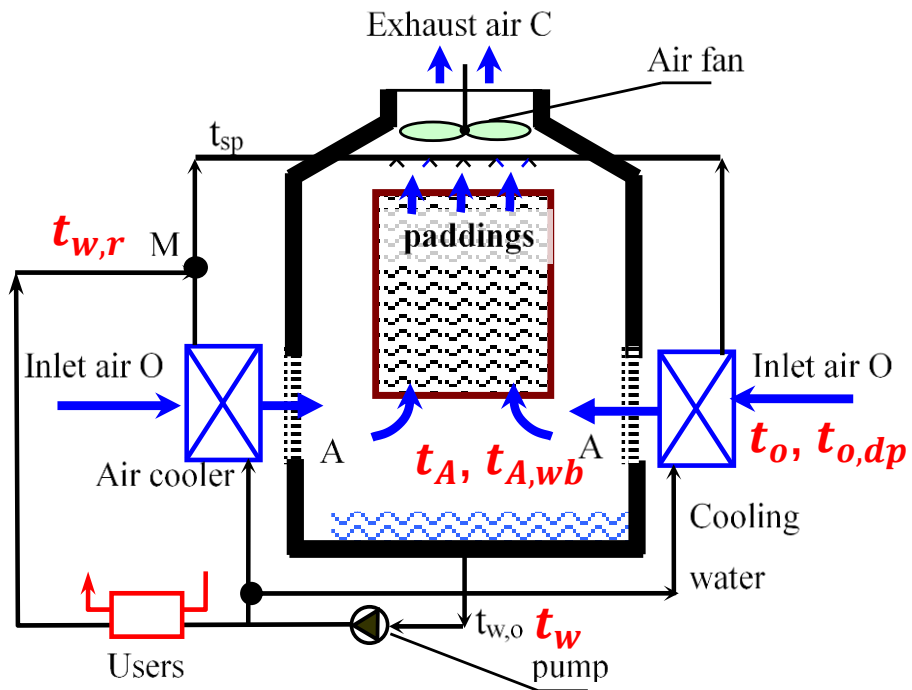
- Define two efficiencies - the evaporative cooling efficiency η_{ev} and the sensible cooling efficiency η_c

$$\eta_c = \frac{t_o - t_A}{t_o - t_{o,dp}}$$

$$\eta_{ev} = \frac{t_{w,r} - t_w}{t_{w,r} - t_{A,wb}}$$

Using η_{dew} as the indicator for IEC water chiller processes

- If only define one efficiency-Dew point temperature efficiency



$$\eta_{dew} = \frac{t_{w,r} - t_w}{t_{w,r} - t_{o,dp}}$$

Thus, t_w could be described as the follow equation:

$$t_w = t_{w,r} - \eta_{dew} * \{t_{w,r} - t_{o,dp}\}$$

t_o : inlet air temperature;

$t_{o,dp}$: inlet air dewpoint temperature;

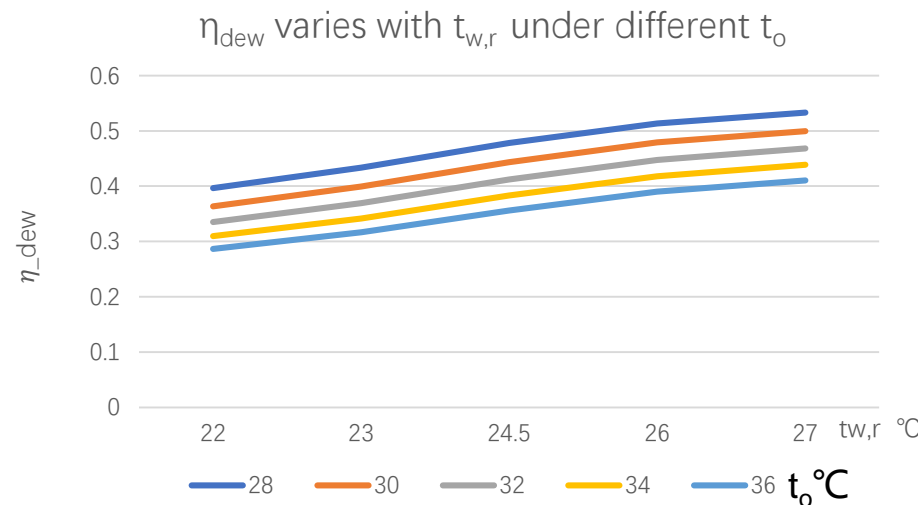
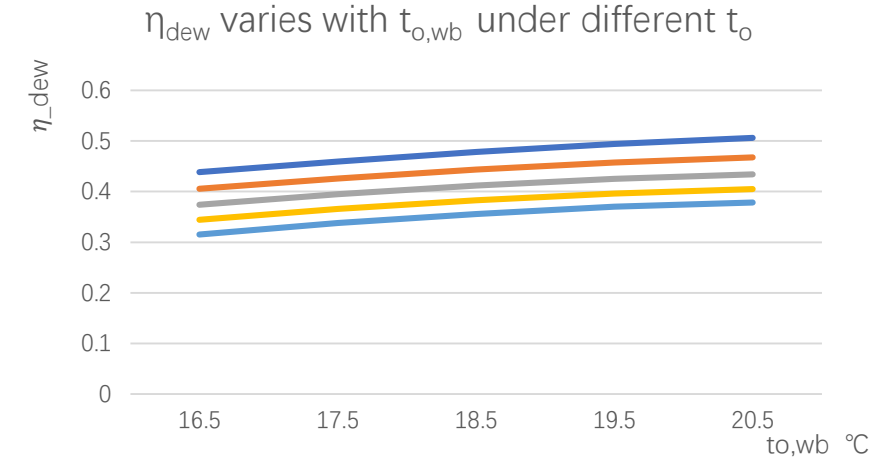
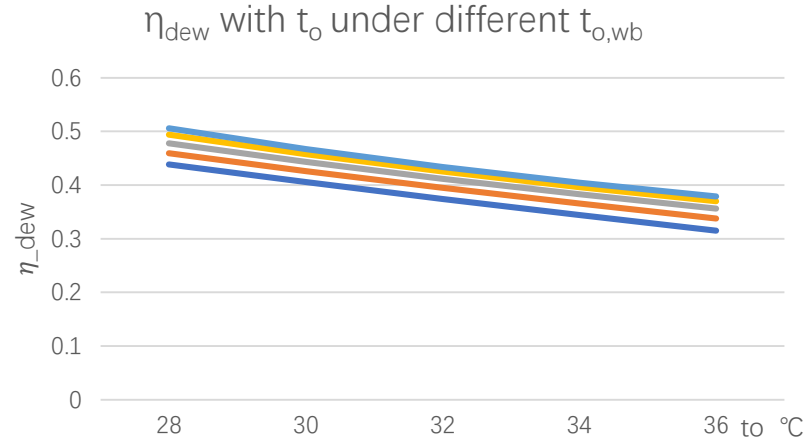
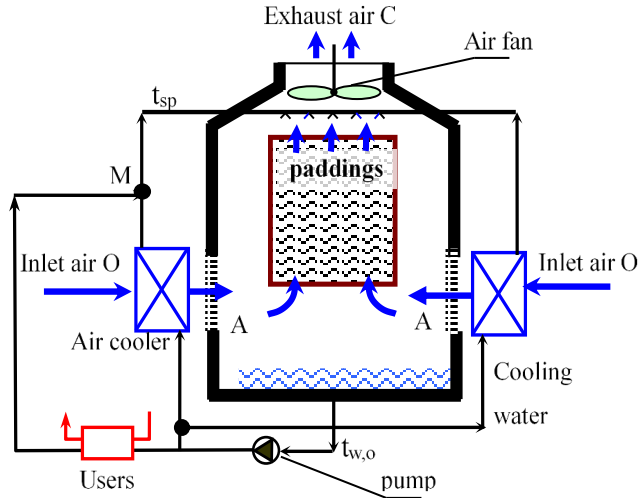
$t_{w,r}$: inlet water temperature;

t_w : outlet water temperature.

Using η_{dew} as the indicator for IEC water chiller processes

- For **parallel-connected** IEC water chillers

$$\eta_{dew} = \frac{t_{w,r} - t_w}{t_{w,r} - t_{O,dp}}$$



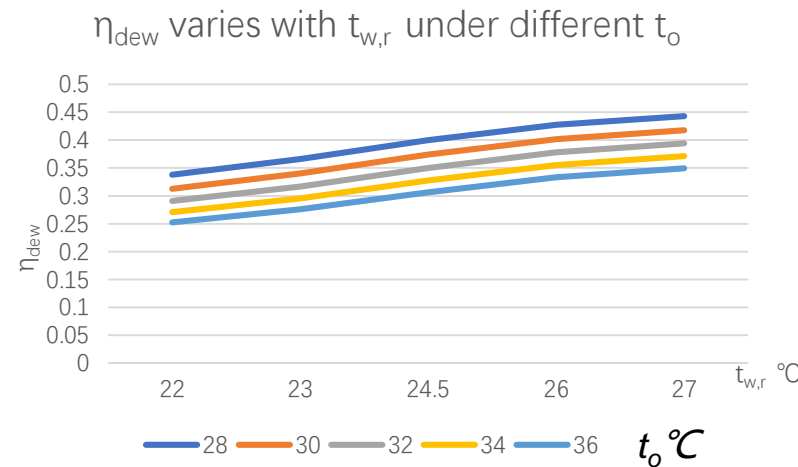
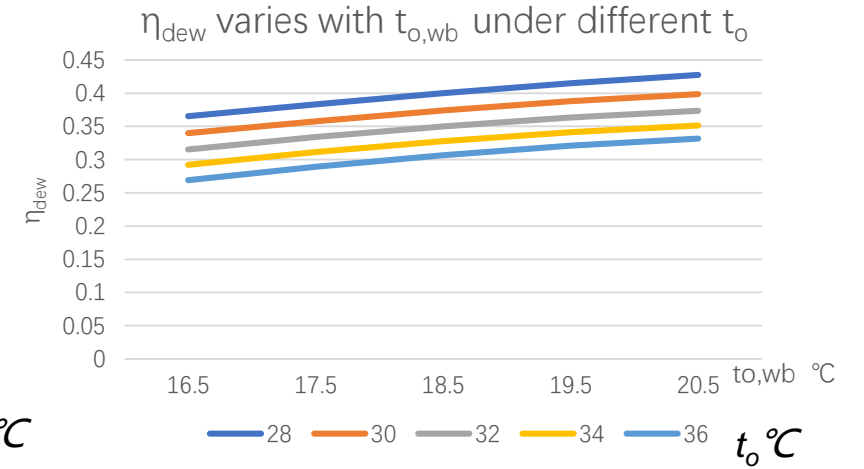
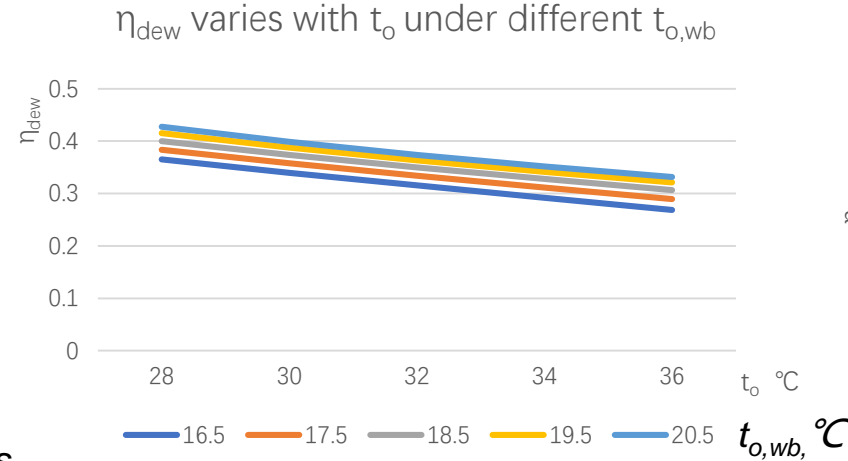
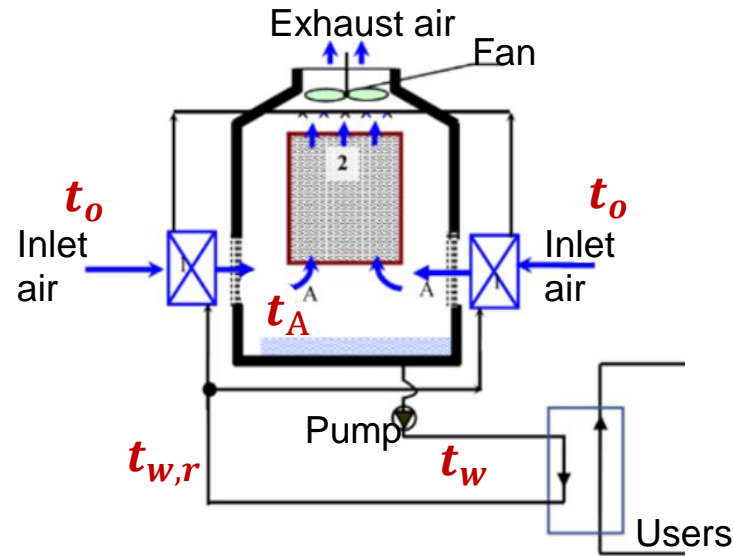
η_{dew} decreases when t_o increases
 η_{dew} increases when $t_{O,wb}$ increases
 η_{dew} increases when $t_{w,r}$ increases

| parameter | design value |
|---|-------------------------|
| inlet air dry-bulb temperature t_o °C | 34^{+2}_{-6} °C |
| inlet air wet-bulb temperature $t_{o,wb}$ | 18.5^{+2}_{-2} °C |
| returned water temperature $t_{w,r}$ | $24.5^{+2.5}_{-2.5}$ °C |
| Flow rate $G_a/G_{w,r}$ | $m=2.25$ |
| capacity of heat exchanger | $Ntu_{ex}=2$ |
| capacity of padding | $Ntu_{padding}=1.5$ |

Using η_{dew} as the indicator for IEC water chiller processes

- For **series-connected** IEC water chillers

$$\eta_{dew} = \frac{t_{w,r} - t_w}{t_{w,r} - t_{O,dp}}$$

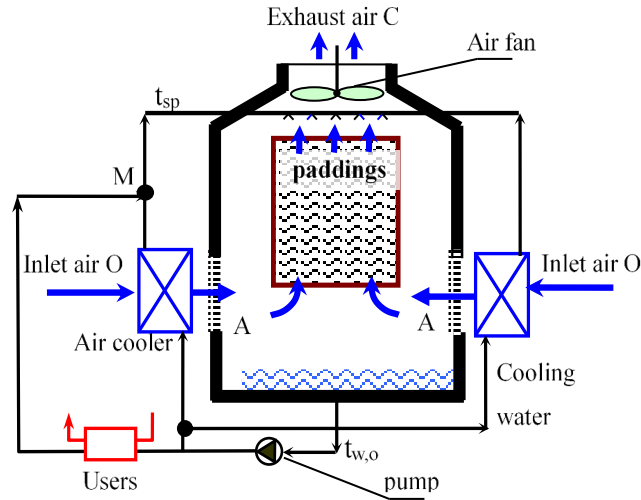


η_{dew} decreases when t_o increases
 η_{dew} increases when $t_{O,wb}$ increases
 η_{dew} increases when $t_{w,r}$ increases

| parameter | design value |
|---|-------------------------|
| inlet air dry-bulb temperature t_o °C | 34^{+2}_{-6} °C |
| inlet air wet-bulb temperature $t_{O,wb}$ | 18.5^{+2}_{-2} °C |
| returned water temperature $t_{w,r}$ | $24.5^{+2.5}_{-2.5}$ °C |
| Flow rate $G_a/G_{w,r}$ | $m=1.5$ |
| capacity of heat exchanger | $Ntu_{ex}=2$ |
| capacity of padding | $Ntu_{padding}=1.5$ |

Using η_{dew} as the indicator for IEC water chiller processes

- For **parallel-connected** IEC water chillers

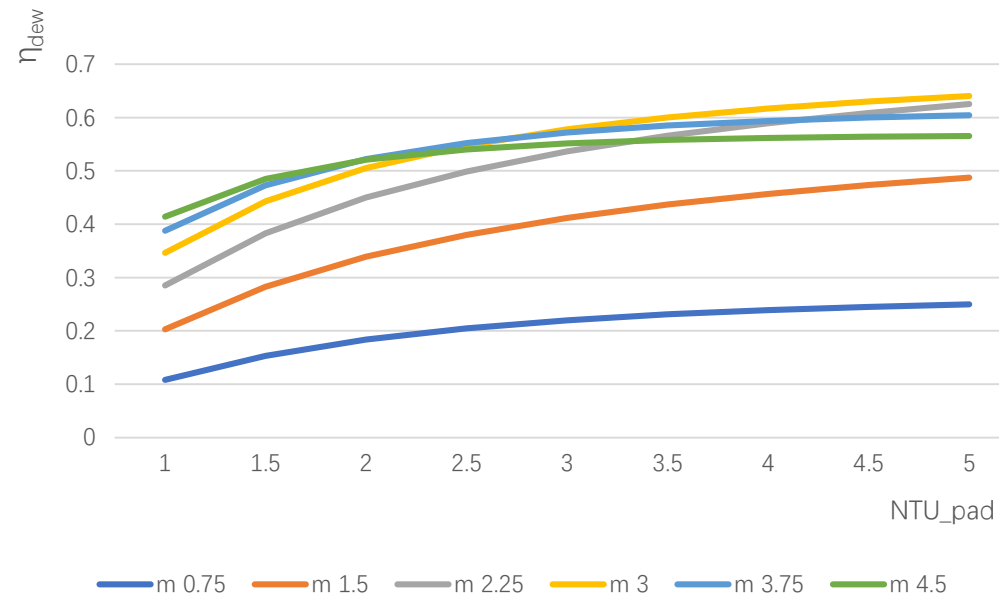


| parameter | design value |
|---|---------------------------|
| inlet air dry-bulb temperature t_o °C | 34°C |
| inlet air wet-bulb temperature $t_{o,wb}$ | 18.5°C |
| returned water temperature $t_{w,r}$ | 24.5°C |
| Flow rate $G_a/G_{w,r}$ | $m = 2.25^{+1.5}_{-1.5}$ |
| capacity of heat exchanger | $NTU_{ex} = 2$ |
| capacity of padding | $NTU_{pad} = 3^{+2}_{-2}$ |

$$m = \frac{G_a}{G_{w,r}}$$

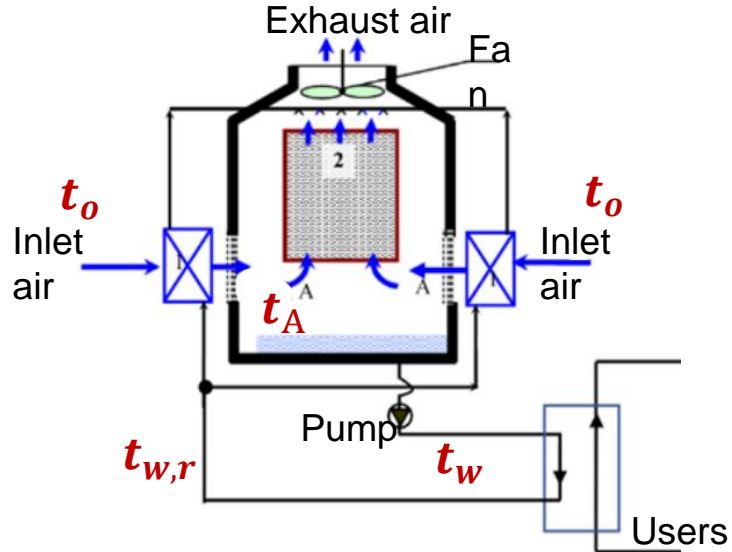
$$NTU_{pad} = \frac{K_s A}{G_a c_{pa}}$$

η_{dew} varies with NTU_{pad} under different m



Using η_{dew} as the indicator for IEC water chiller processes

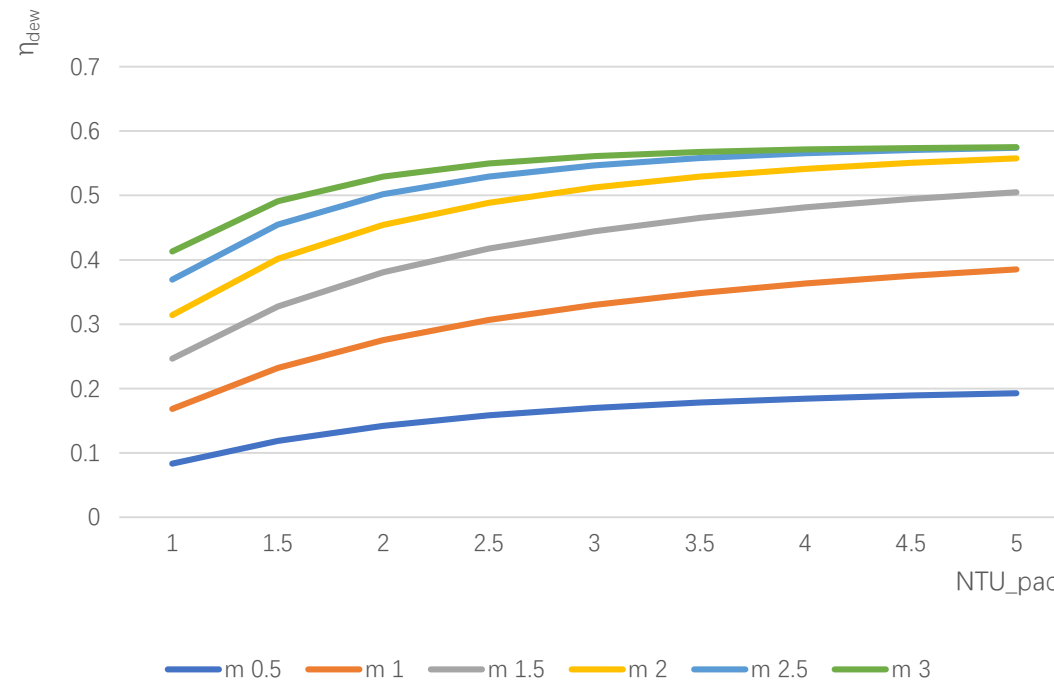
- For **series-connected** IEC water chillers



$$m = \frac{G_a}{G_{w,r}}$$

$$NTU_{pad} = \frac{K_s A}{G_a c_{pa}}$$

η_{dew} varies with NTU_{pad} under different m

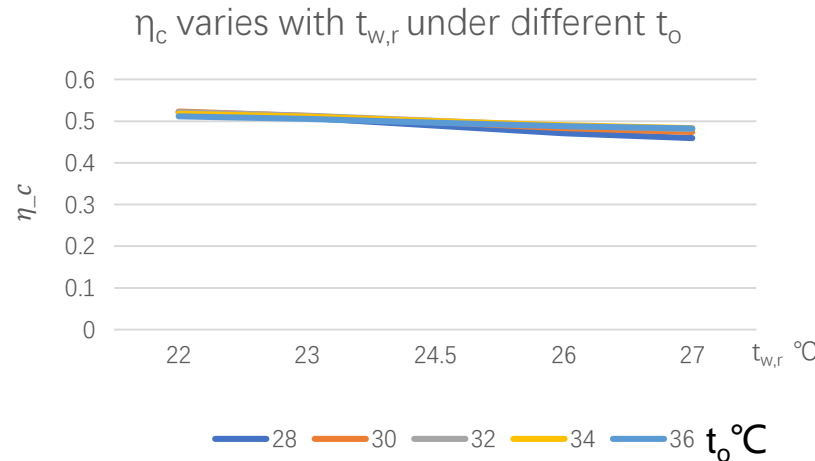
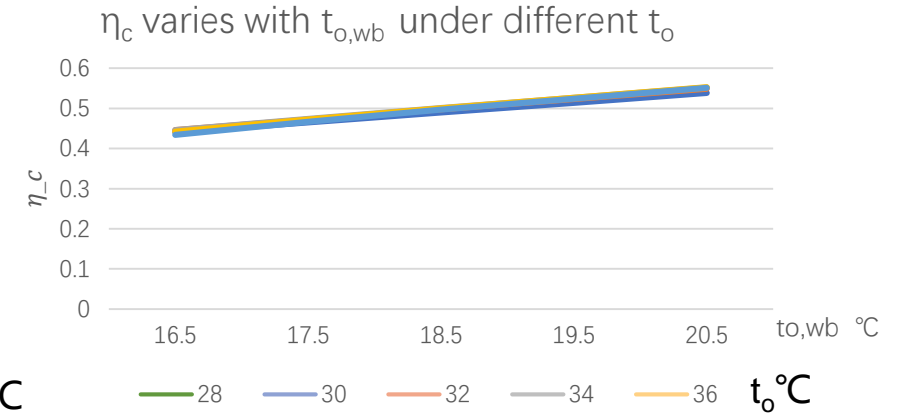
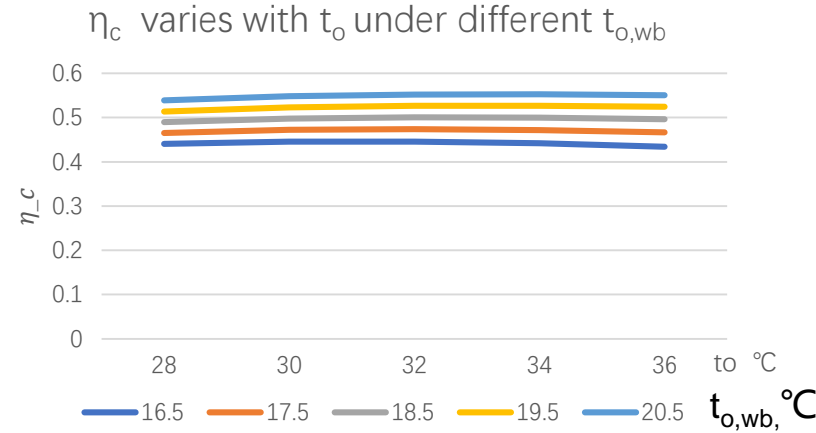
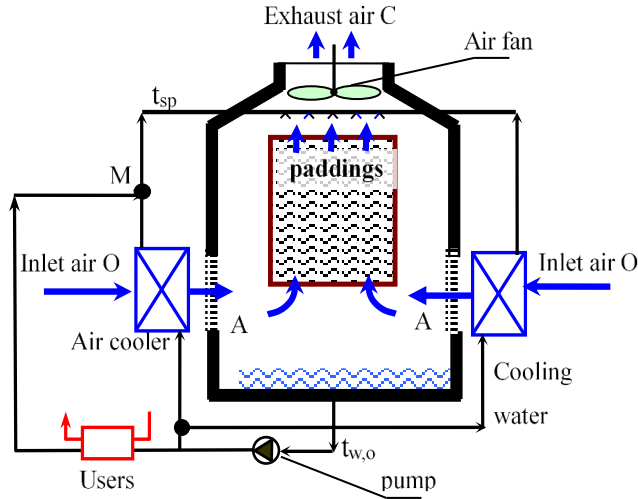


| parameter | design value |
|---|---------------------------|
| inlet air dry-bulb temperature t_o °C | 34°C |
| inlet air wet-bulb temperature $t_{o,wb}$ | 18.5°C |
| returned water temperature $t_{w,r}$ | 24.5°C |
| Flow rate $G_a/G_{w,r}$ | $m = 1.5^{+1.5}_{-1}$ |
| capacity of heat exchanger | $NTU_{ex} = 2$ |
| capacity of padding | $NTU_{pad} = 3^{+2}_{-2}$ |

Using η_c & η_{ev} as the indicators for IEC water chiller processes

- For **parallel-connected** IEC water chillers

$$\eta_c = \frac{t_o - t_A}{t_o - t_{o,dp}}$$

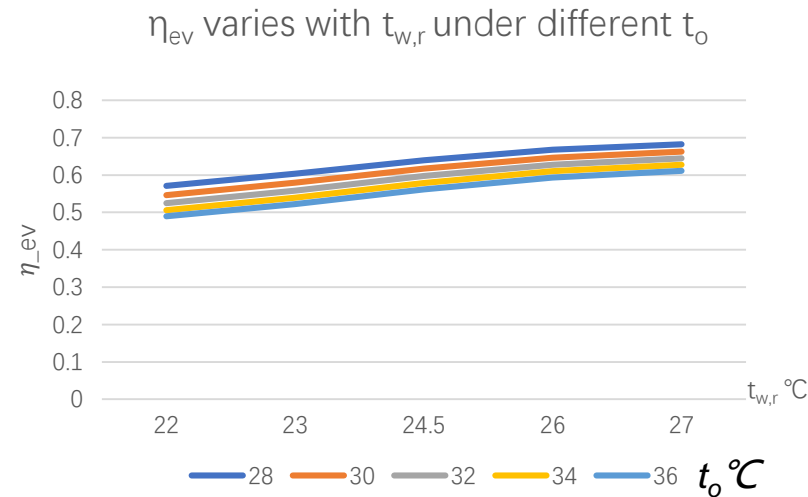
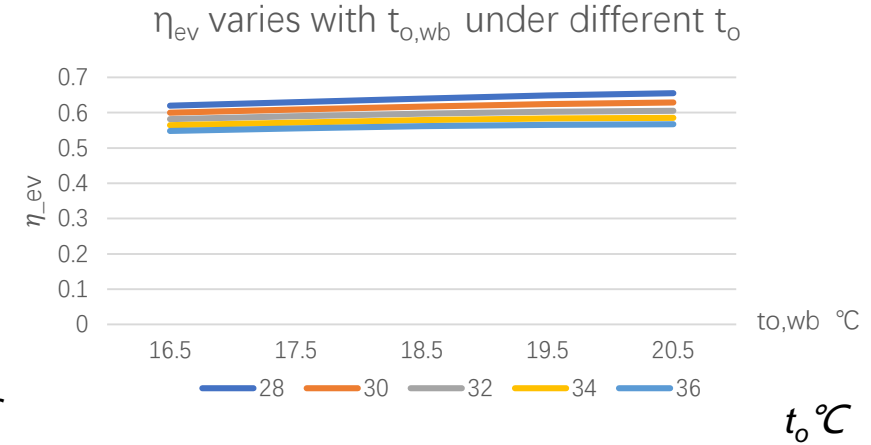
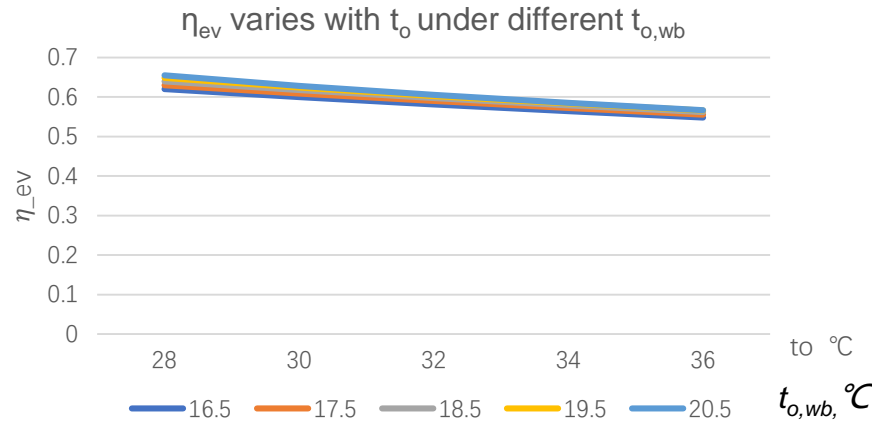
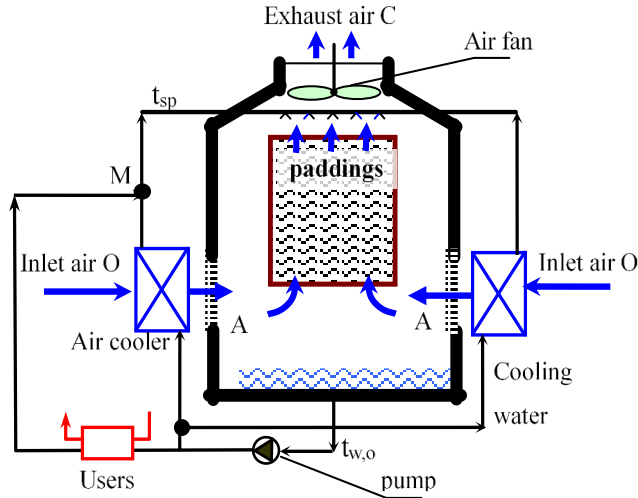


| parameter | design value |
|---|-------------------------|
| inlet air dry-bulb temperature t_o °C | 34^{+2}_{-6} °C |
| inlet air wet-bulb temperature $t_{o,wb}$ | 18.5^{+2}_{-2} °C |
| returned water temperature $t_{w,r}$ | $24.5^{+2.5}_{-2.5}$ °C |
| Flow rate $G_a/G_{w,r}$ | $m=2.25$ |
| capacity of heat exchanger | $Ntu_{ex}=2$ |
| capacity of padding | $Ntu_{padding}=1.5$ |

Using η_c & η_{ev} as the indicators for IEC water chiller processes

- For **parallel-connected** IEC water chillers

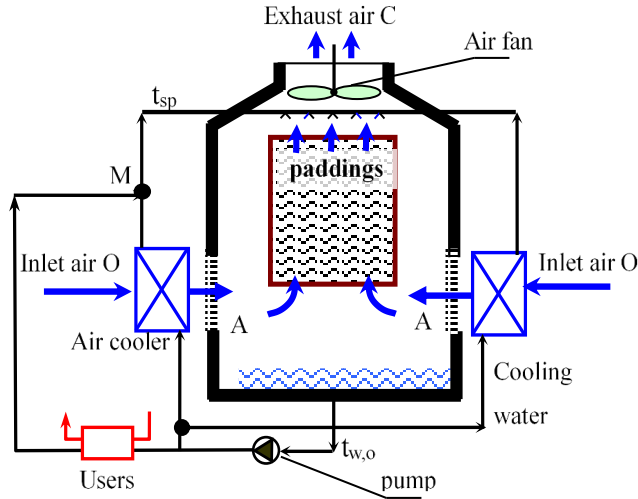
$$\eta_{ev} = \frac{t_{w,r} - t_w}{t_{w,r} - t_{A,wb}}$$



| parameter | design value |
|---|-------------------------|
| inlet air dry-bulb temperature t_o °C | 34_{-6}^{+2} °C |
| inlet air wet-bulb temperature $t_{o,wb}$ | 18.5_{-2}^{+2} °C |
| returned water temperature $t_{w,r}$ | $24.5_{-2.5}^{+2.5}$ °C |
| Flow rate $G_a/G_{w,r}$ | $m=2.25$ |
| capacity of heat exchanger | $Ntu_{ex}=2$ |
| capacity of padding | $Ntu_{padding}=1.5$ |

Using η_c & η_{ev} as the indicators for IEC water chiller processes

- For **parallel-connected** IEC water chillers

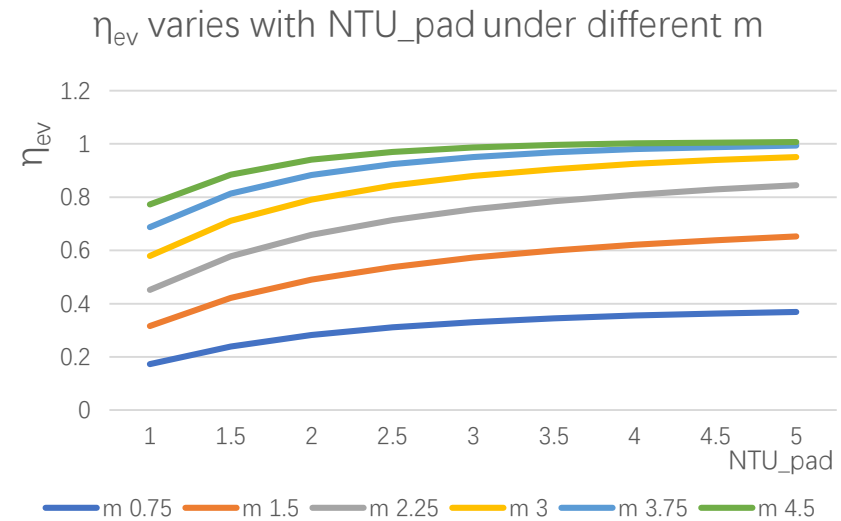
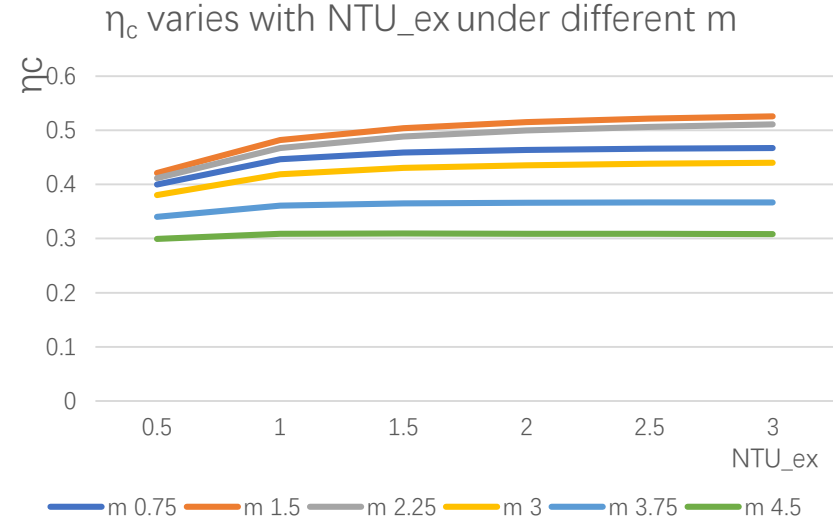


$$m = \frac{G_a}{G_{w,r}}$$

$$NTU_{ex} = \frac{KA}{G_a c_{pa}}$$

$$NTU_{pad} = \frac{K_s A}{G_a c_{pa}}$$

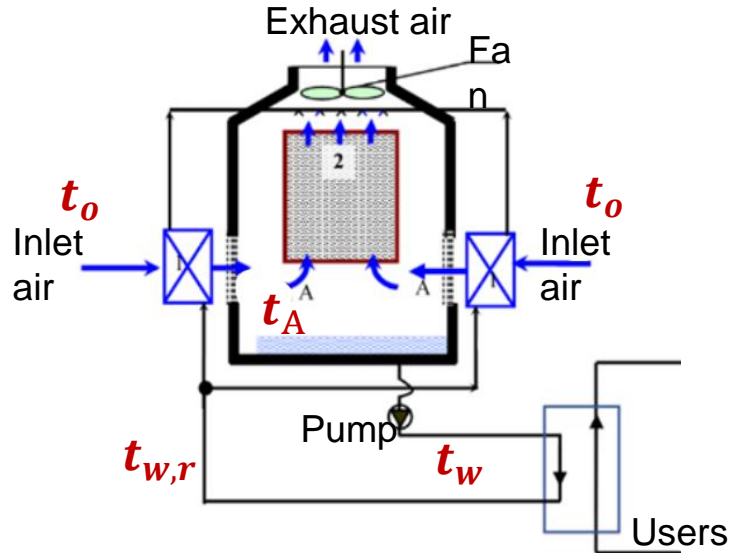
| parameter | design value |
|---|---------------------------------|
| inlet air dry-bulb temperature t_o °C | 34°C |
| inlet air wet-bulb temperature $t_{o,wb}$ | 18.5°C |
| returned water temperature $t_{w,r}$ | 24.5 °C |
| Flow rate $G_a/G_{w,r}$ | $m = 2.25^{+2.25}_{-1.5}$ |
| capacity of heat exchanger | $NTU_{ex} = 2^{+1}_{-1.5}$ |
| capacity of padding | $NTU_{pad} = 1.5^{+3.5}_{-0.5}$ |



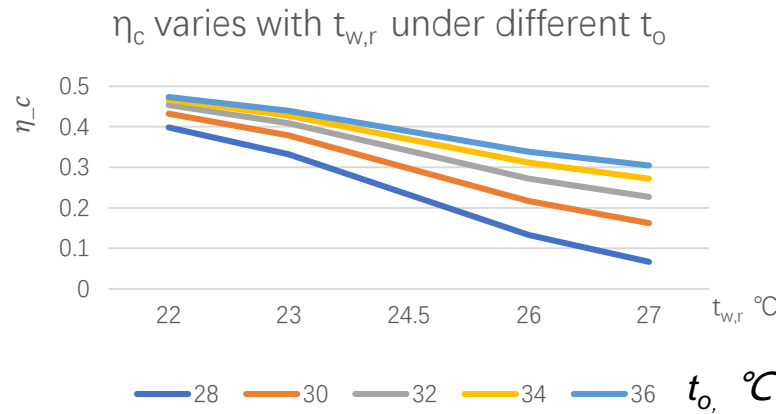
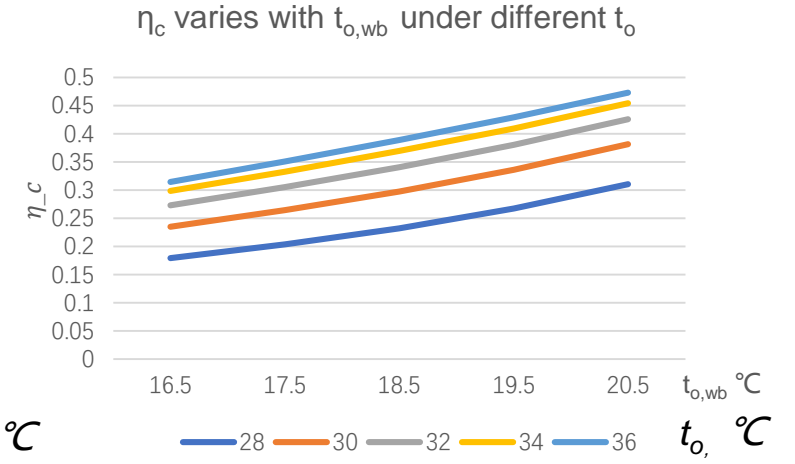
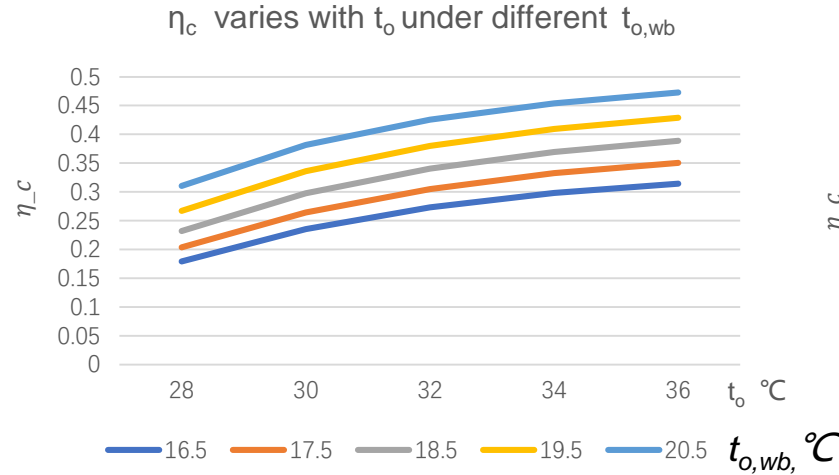
Using η_c & η_{ev} as the indicators for IEC water chiller processes

- For **series-connected** IEC water chillers

$$\eta_c = \frac{t_o - t_A}{t_o - t_{o,dp}}$$



| parameter | design value |
|---|-------------------------|
| inlet air dry-bulb temperature t_o °C | 34^{+2}_{-6} °C |
| inlet air wet-bulb temperature $t_{o,wb}$ | 18.5^{+2}_{-2} °C |
| returned water temperature $t_{w,r}$ | $24.5^{+2.5}_{-2.5}$ °C |
| Flow rate $G_a/G_{w,r}$ | $m=1.5$ |
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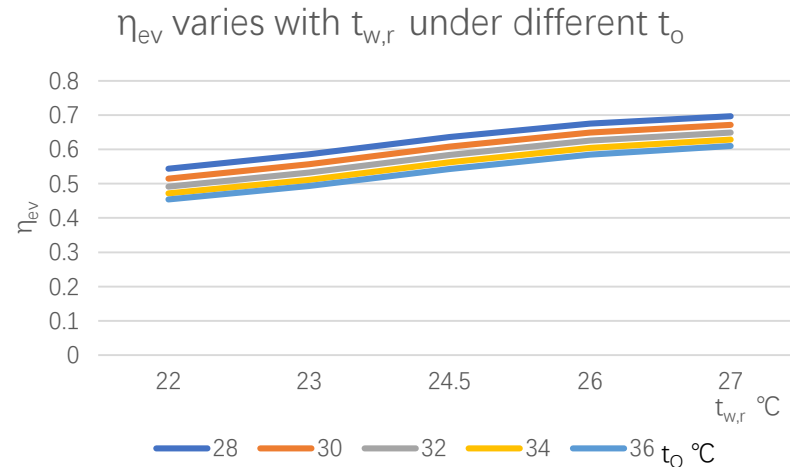
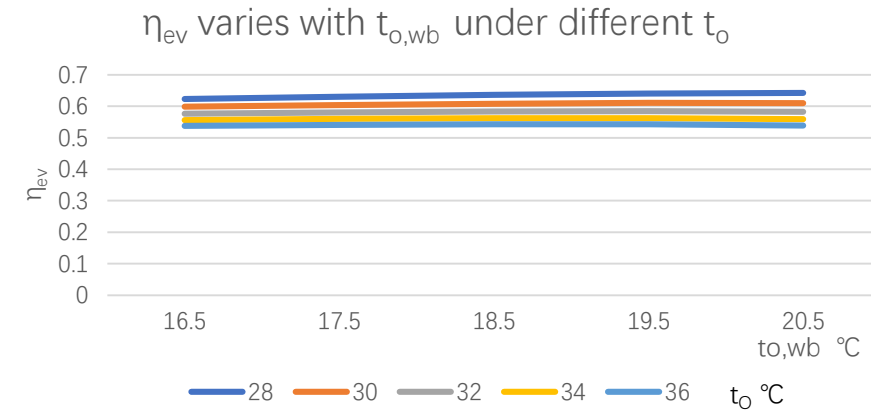
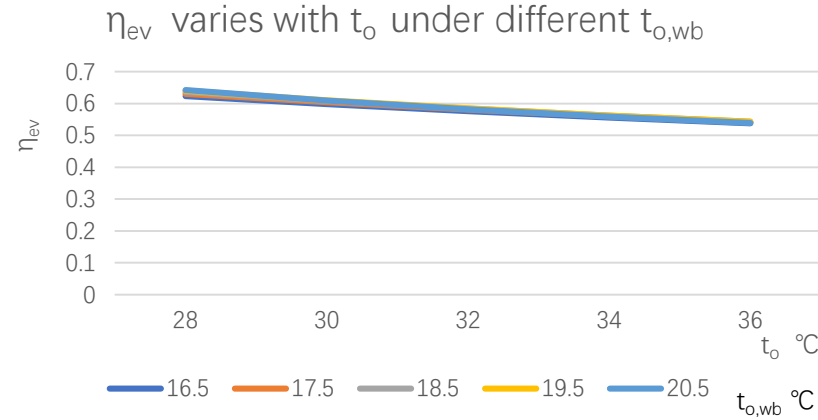
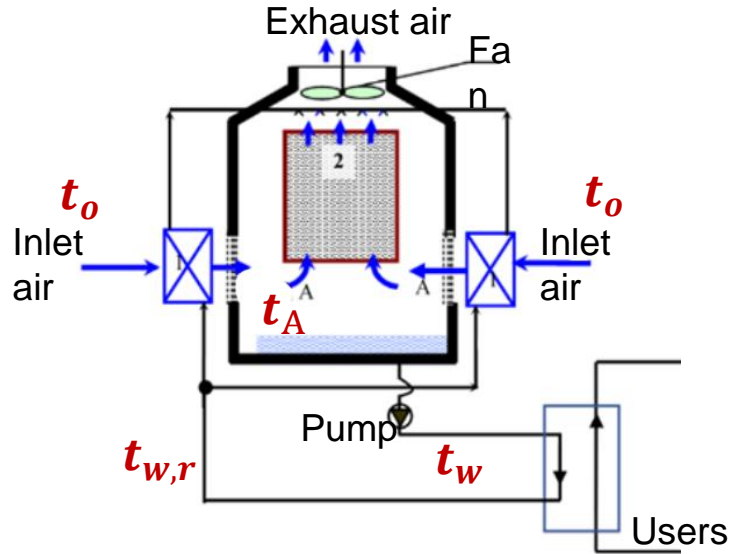


η_c increases when t_o increases
 η_c increases when $t_{o,wb}$ increases
 η_c decreases when $t_{w,r}$ increases

Using η_c & η_{ev} as the indicators for IEC water chiller processes

- For **series-connected** IEC water chillers

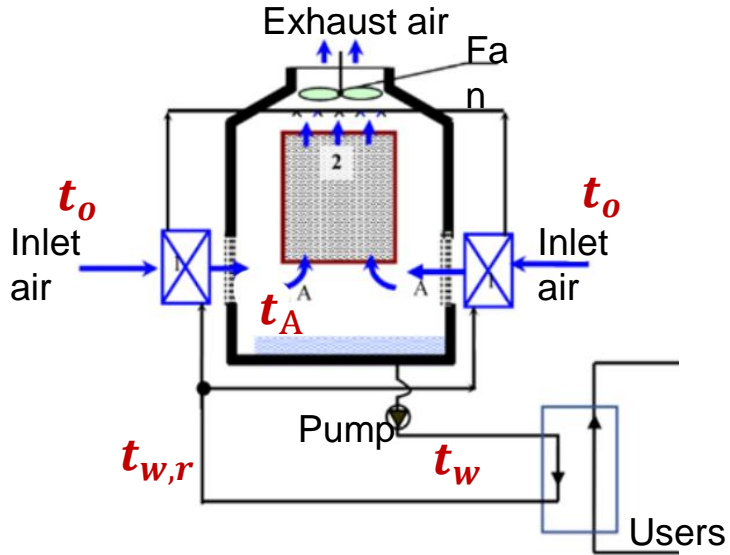
$$\eta_{ev} = \frac{t_{w,r} - t_w}{t_{w,r} - t_{A,wb}}$$



| parameter | design value |
|---|-------------------------|
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| Flow rate $G_a/G_{w,r}$ | $m=1.5$ |
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Using η_c & η_{ev} as the indicators for IEC water chiller processes

- For **series-connected** IEC water chillers

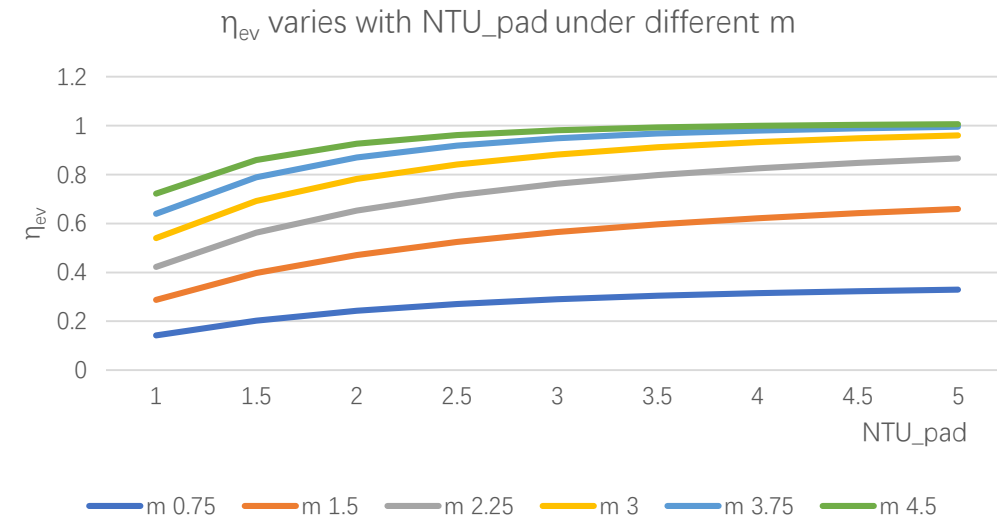
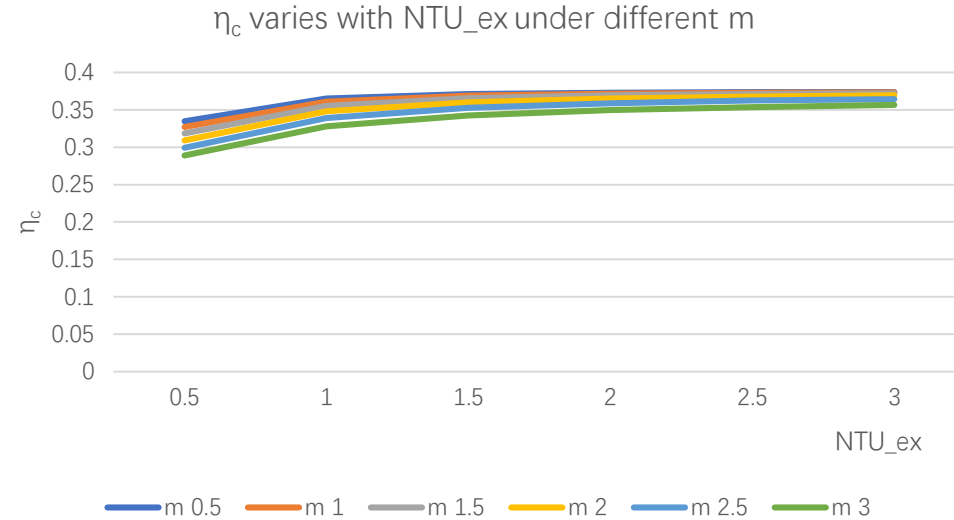


$$m = \frac{G_a}{G_{w,r}}$$

$$NTU_{ex} = \frac{KA}{G_a c_{pa}}$$

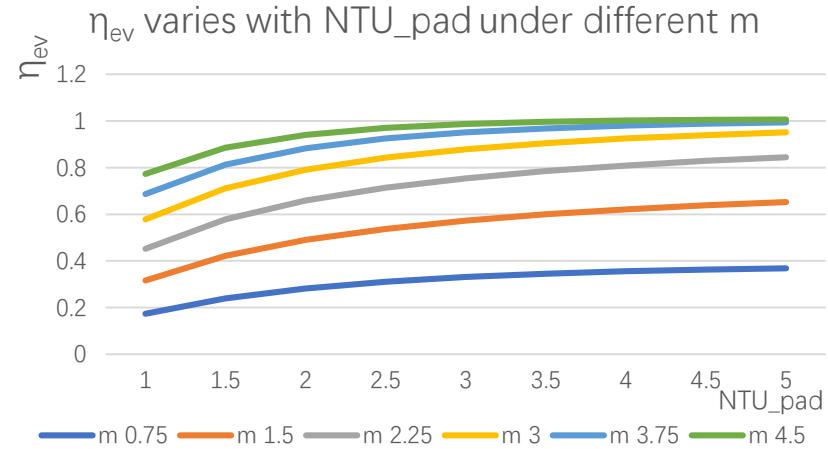
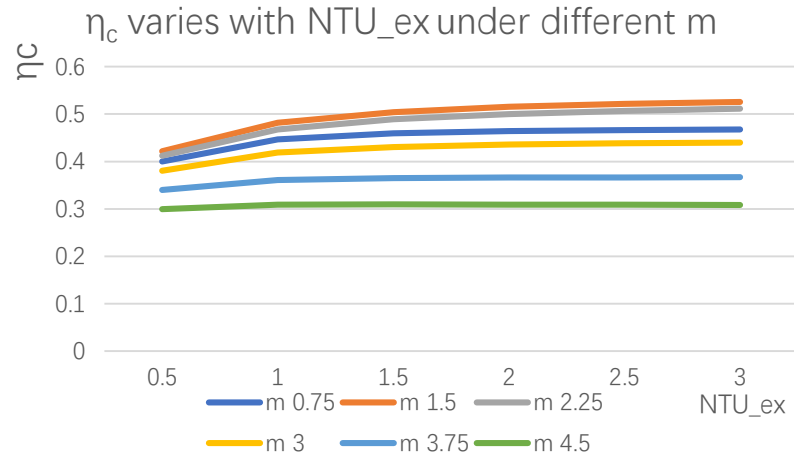
$$NTU_{pad} = \frac{K_s A}{G_a c_{pa}}$$

| parameter | design value |
|---|---------------------------------|
| inlet air dry-bulb temperature t_o °C | 34°C |
| inlet air wet-bulb temperature $t_{o,wb}$ | 18.5 °C |
| returned water temperature $t_{w,r}$ | 24.5 °C |
| Flow rate $G_a/G_{w,r}$ | $m = 1.5^{+1.5}_{-1}$ |
| capacity of heat exchanger | $NTU_{ex} = 2^{+1}_{-1.5}$ |
| capacity of padding | $NTU_{pad} = 1.5^{+3.5}_{-0.5}$ |

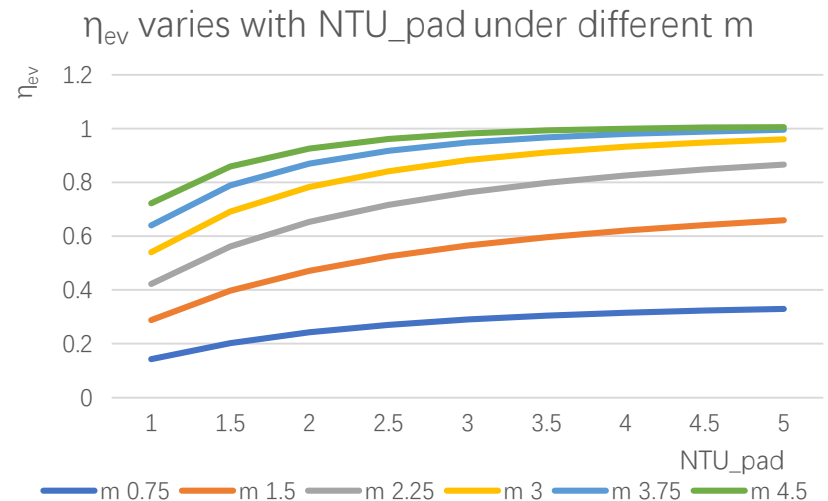
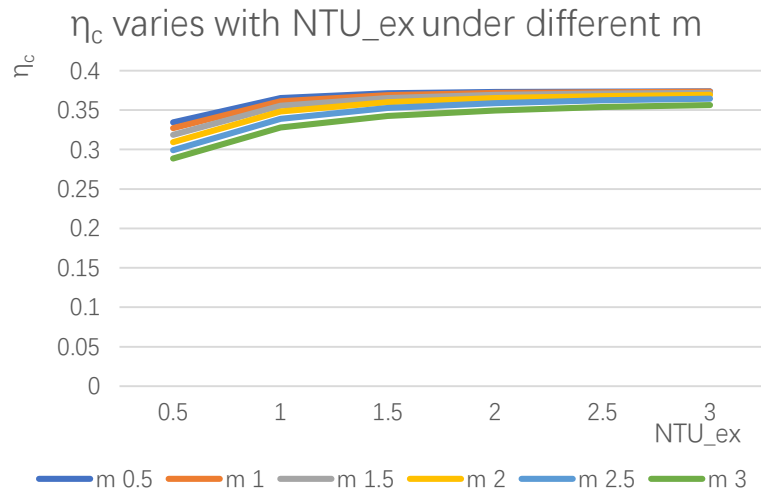


Summary

- For **parallel-connected** IEC water chillers, the evaporative cooling efficiency η_{ev} and the sensible cooling efficiency η_c are more suitable with a stable performance under various climate conditions.



- For **series-connected** IEC water chillers, all three indicators are not completely stable with $t_o, t_{o,wb}, t_{w,r}$. NTU-m- η curves are used as a reference. Maybe linear fitting?



**Thank you very much
for your attention!**